



Royal Netherlands
Meteorological Institute
*Ministry of Infrastructure
and Environment.*



EarthCARE level 2 development projects APRIL, CLARA and DORSY
final presentation

M-AOT processor and M-AOT product developed in APRIL

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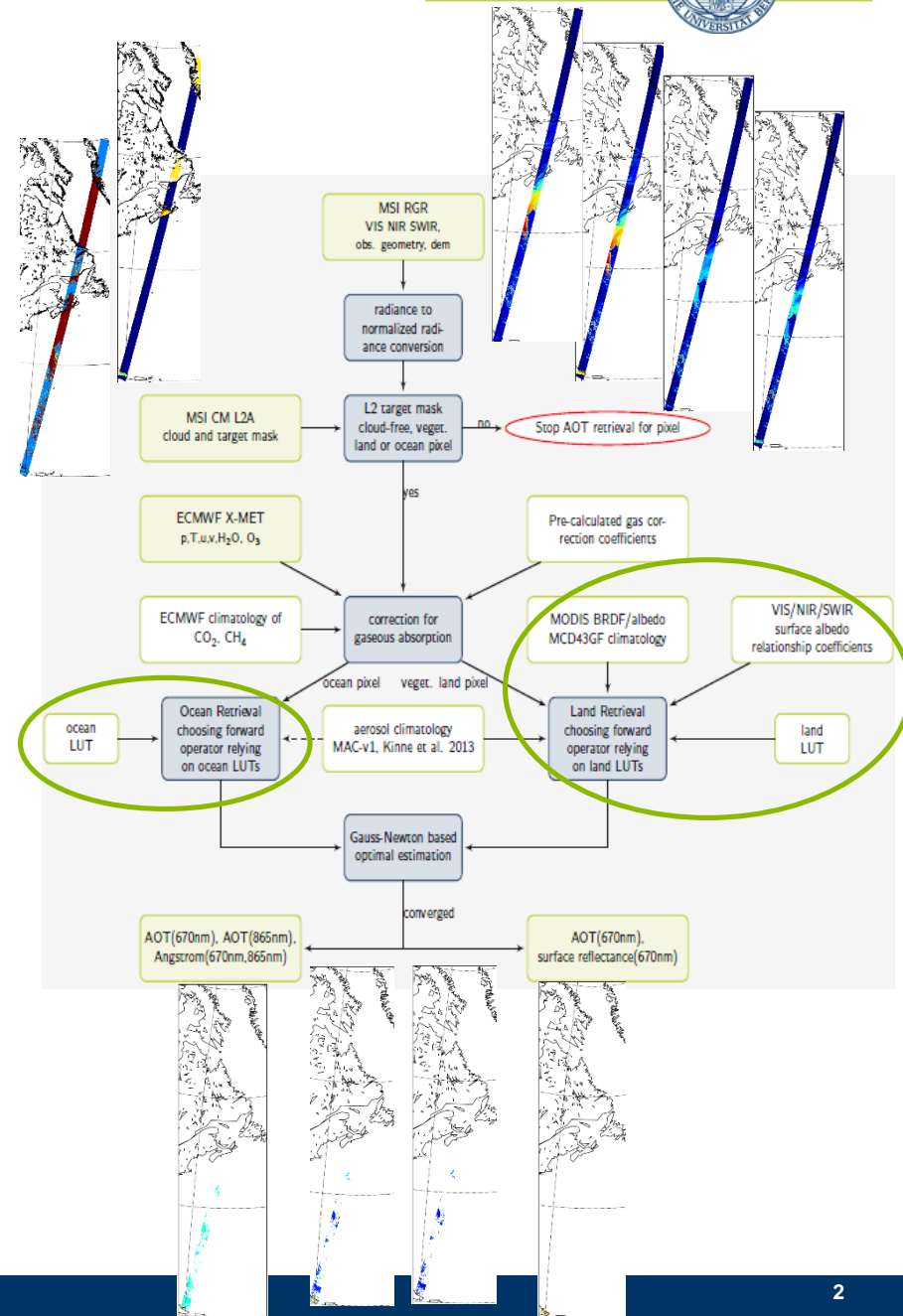
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M-AOT v8.x overview

- MSI stand-alone aerosol processor
- Daytime and cloud-free only
- Output resolution on native MSI grid
- Purpose: offer information on horizontal aerosol distribution complementing vertical nadir information from ATLID
- Optimal estimation based retrieval approach of aerosol optical thickness (AOT) over ocean, and where possible land, at 670 nm and over ocean at 865 nm
- Measured signal will be corrected for gaseous absorption in advance

$$T_{\text{gas}}(\lambda) = \exp(-\text{AMF} \cdot (a(\lambda) + b(\lambda) \cdot \text{gas} + c(\lambda) \cdot \text{gas}^2))$$
 used correction coefficients are based on line-by-line code included in MOMO (Doppler et al. 2014) applying HITRAN 2012 (Rothman et al., 2014) database
- Forward operators consist of interpolation in LUTs created with FUB in-house radiative transfer model MOMO (Hollstein and Fischer, 2012, Doppler et al. 2014)
- LUT definition / assumptions: 25 aerosol component mixings via AOT ratios of the four basic HETEAC types (Wandinger et al. 2016)



- Assumed signal dependence $\rho_\lambda(\phi_{rel}, \theta_{sun}, \theta_{sat}, \tau_{aer}, \alpha_\lambda, p, mix_{aer})$
- Aerosol component mixing chosen from MAC v1 (Kinne et al., 2013) climatology

Land retrieval – sensitivity

Assumptions:

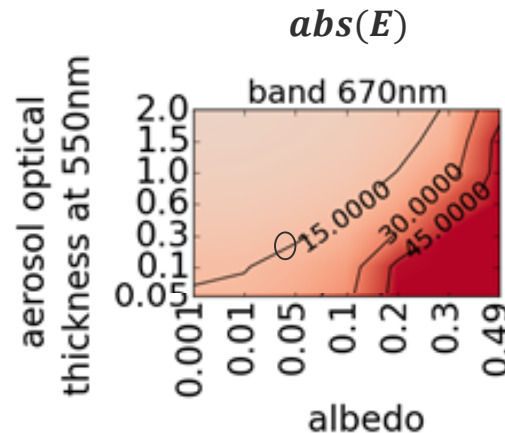
- other parameters are perfectly known
- One channel at a time considered

$$\rho(\tau, \alpha) = \rho(\tau_0, \alpha_0) + \frac{\partial \rho}{\partial \tau} \Delta \tau + \frac{\partial \rho}{\partial \alpha} \Delta \alpha$$

- Error propagation factor E (worst case):
Assuming that $\rho(\tau, \alpha) = \rho(\tau_0, \alpha_0)$, $\Delta \rho = 0$:
 $\Delta \tau = -E \Delta \alpha$, $E = (\partial \rho / \partial \alpha) / (\partial \rho / \partial \tau)$

→ Assuming state: AOT = 0.2, albedo = 0.05

absolute error propagation factor of ~15 -> **albedo error of 0.01** would lead to **AOT error of 0.15**



Case study

- HETEAC fine mode less absorbing aerosol
- SZA=40°
- RAA=140°
- VZA=0°
- Pressure=1013.25hPa

→ Need for climatological albedo update that represents the current surface state reasonably well

- Optimal estimation measurement \vec{y} and state vector \vec{x} :

$$\vec{y} = \begin{pmatrix} \rho_{VIS} \\ \rho_{SWIR1} \\ \rho_{SWIR2} \end{pmatrix}, \vec{x} = \begin{pmatrix} \tau_{aer} \\ \alpha_{SWIR2} \\ NDVI_{SWIR} \end{pmatrix}$$
- Forward operator approach:
 - Usage of surface parameterization
 - linear interpolation in LUTs
 - inverse distance weighting of aerosol component mixing

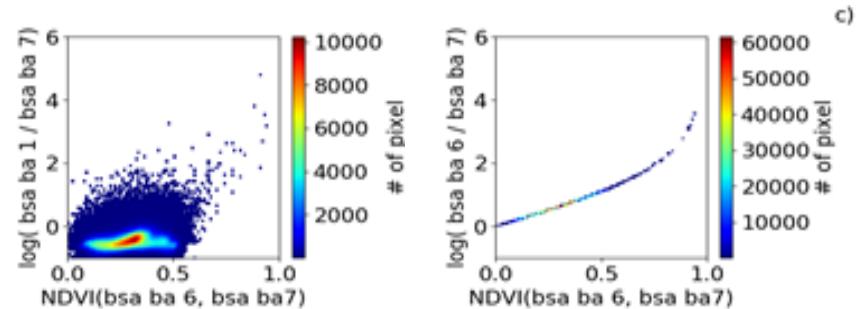
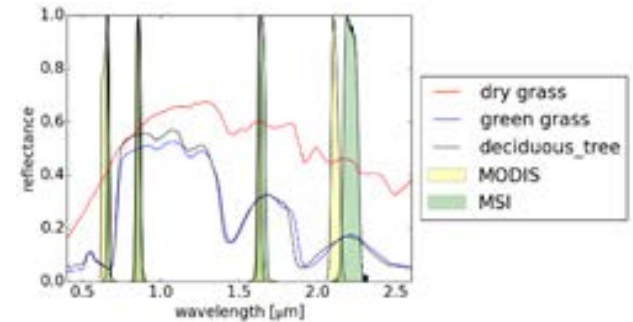
Land retrieval – empirical surface parameterization

- MODIS BRDF/albedo climatology (provided by Environment Canada) has been analysed and used to create a parameterization
- Estimation of VIS, SWIR-1 albedo using SWIR-2 black sky albedo and greenness:

$$\alpha_{\lambda} = \alpha_{SWIR2} \cdot \exp(a_{\lambda,SWIR2} NDVI_{SWIR} + b_{\lambda,SWIR2} + c_{\lambda,SWIR2}),$$

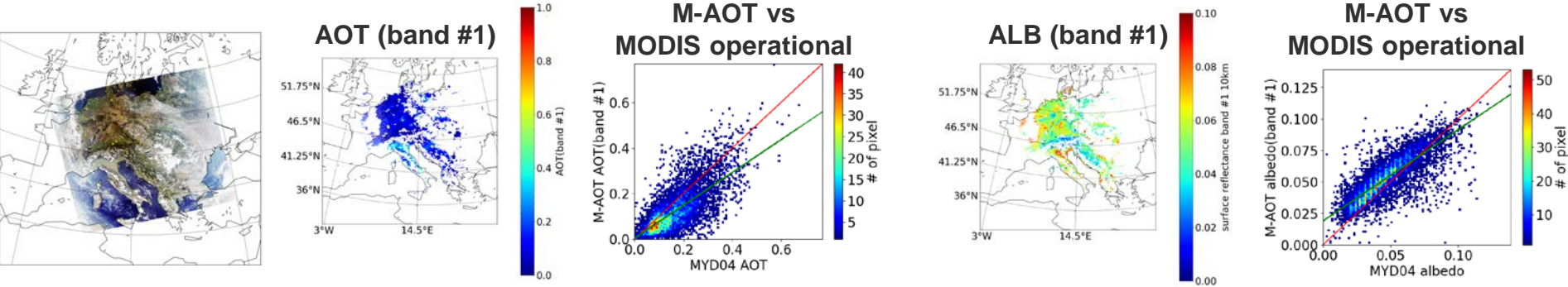
where

- $a_{\lambda,SWIR2}, b_{\lambda,SWIR2}, c_{\lambda,SWIR2}$ stored in LUT
- greenness dependence via $NDVI_{SWIR} = \frac{\rho_{SWIR1} - \rho_{SWIR2}}{\rho_{SWIR1} + \rho_{SWIR2}}$
- dependent on SZA, surface biome (IGBP)

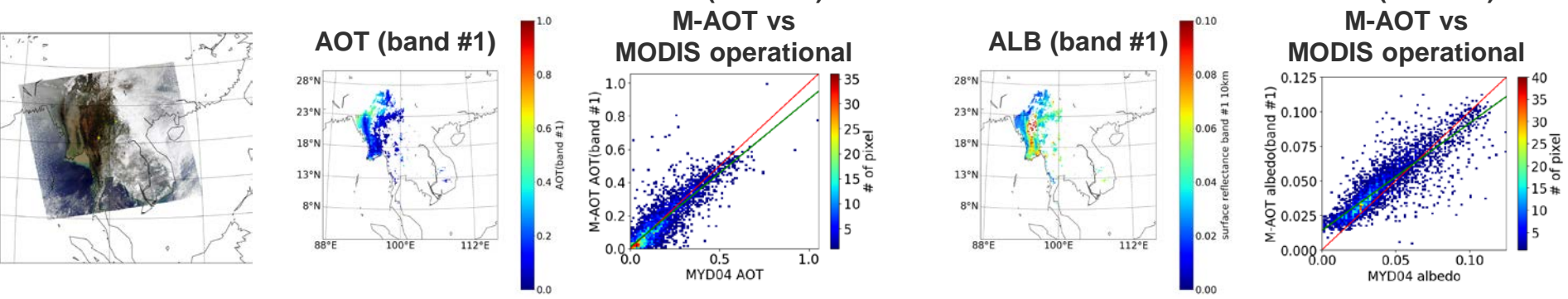


MODIS input based M-AOT LAND retrieval verification

Europe - MYDX.A2016257.1150.006.*

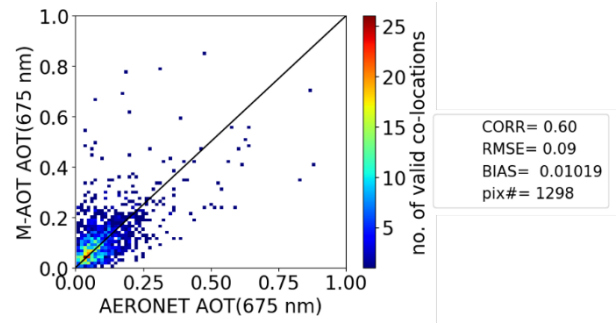


Southeast Asia - MYDX.A2018031.0640.006.*



Verification using M-AOT processed MODIS scenes and comparison with AERONET for 1298 match-ups:

- time difference of 15 minutes
 - spatial distance of 6 km
- shows reasonable agreement



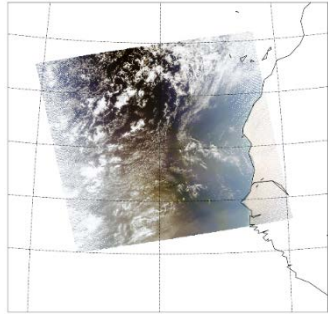
- Assumed signal dependence: $\rho_\lambda(\phi_{rel}, \theta_{sun}, \theta_{sat}, \tau_{aer}, WS, p, mix_{aer})$
- Aerosol component mixing chosen from MAC v1 (Kinne et al., 2013) climatology
- Ocean surface is parameterized via wind speed following Cox and Munk (1954)
- Strong glint areas excluded from retrieval
- Optimal estimation measurement \vec{y} and state vector \vec{x} :

$$\vec{y} = \begin{pmatrix} \rho_{VIS} \\ \rho_{NIR} \\ \rho_{SWIR1} \\ \rho_{SWIR2} \end{pmatrix}, \quad \vec{x} = \begin{pmatrix} \tau_{aer} \\ WS \end{pmatrix}$$

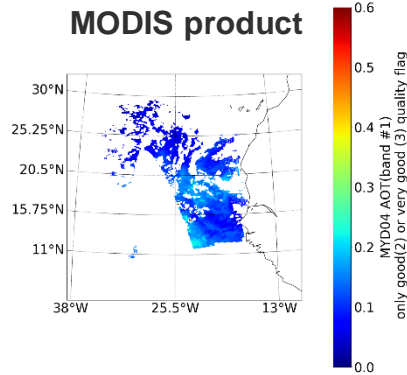
- *currently under development:*
usage of aerosol component mixing based best fit in operational environment that fulfils the runtime requirement
 - development approach
 - optimal estimation of AOT for all 25 pre-defined aerosol component mixings
 - choosing the state vector for which the root-mean-squared error between forward simulated measurement and measurement is lowest

MODIS input based M-AOT OCEAN retrieval verification

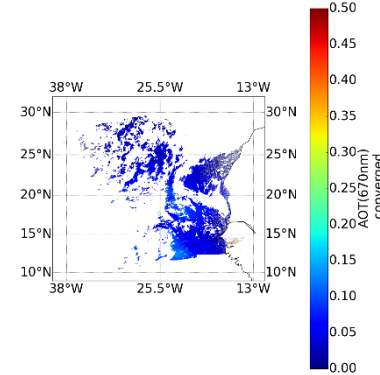
MYDX.A2007344.1500.006.*



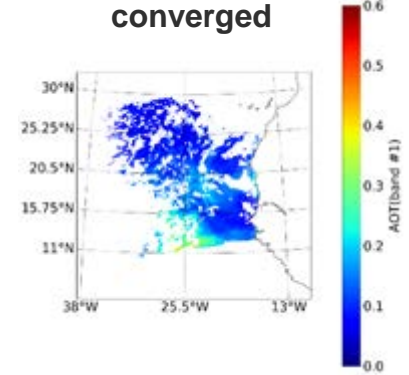
Official MODIS product



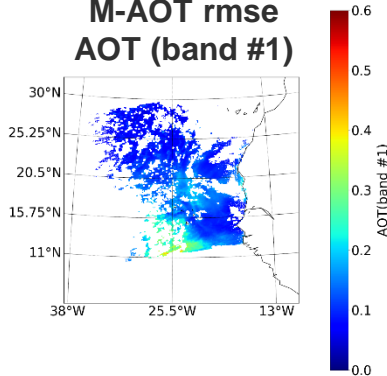
M-AOT default



M-AOT rmse approach converged

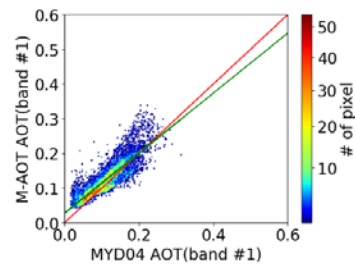


M-AOT rmse AOT (band #1)

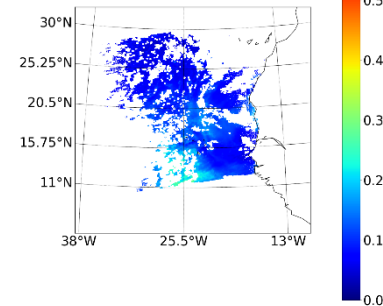


M-AOT rmse approach converged

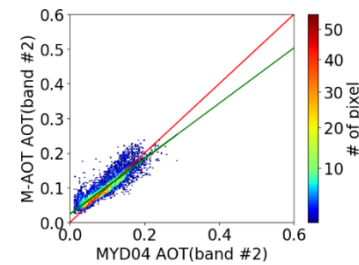
AOT (band #1) M-AOT rmse vs MODIS operational



M-AOT rmse AOT (band #2)

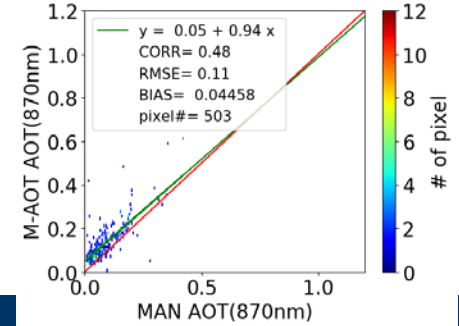
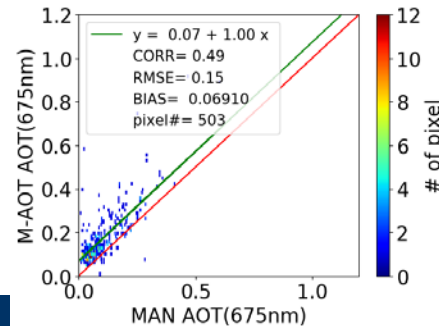


AOT (band #2) M-AOT rmse vs MODIS operational



Verification using M-AOT-rmse processed MODIS scenes and comparison with Maritime Aerosol Network (MAN) for 503 match-ups:

- time difference of 30 minutes
- spatial distance of 0.1° shows reasonable agreement



ECSIM nominal test scenes

- Current used ecsim nominal test scenes for Halifax, Halifax aerosol, Baja and Hawaii

Halifax

- ECA_EXAA_MSI_RGR_1C_20241231T183450Z_20201125T180000Z_39316D
- ECA_EXAA_MSI_CM__2A_20241231T183452Z_20201204T094523Z_39316D

Halifax aerosol

- ECA_EXAA_MSI_RGR_1C_20241231T185624Z_20191029T180000Z_39316D
- ECA_EXAA_MSI_CM__2A_20241231T233450Z_20200108T082724Z_39316D

Baja

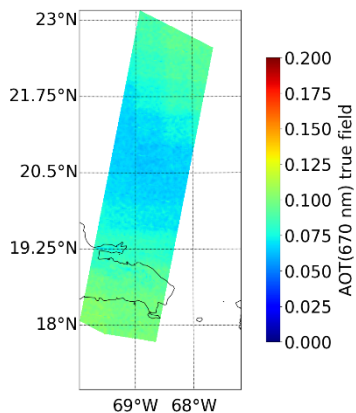
- ECA_EXAA_MSI_RGR_1C_20250410T213955Z_20201125T143000Z_40874D
- ECA_EXAA_MSI_CM__2A_20250410T213958Z_20201204T095038Z_40874D

Hawaii

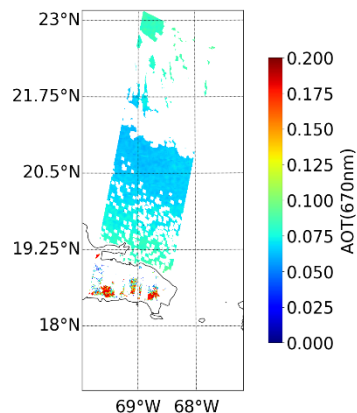
- ECA_EXAA_MSI_RGR_1C_20250625T005649Z_20201026T180000Z_42043E
- ECA_EXAA_MSI_CM__2A_20250625T005649Z_20201204T095224Z_42043E

Halifax MSI_RGR_1C v 20201125

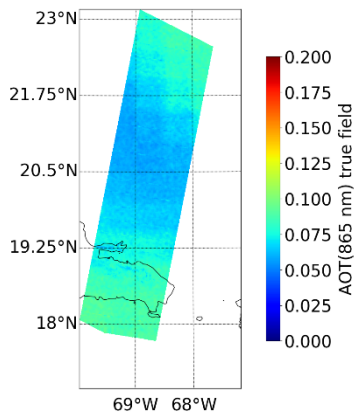
true AOT 670 nm



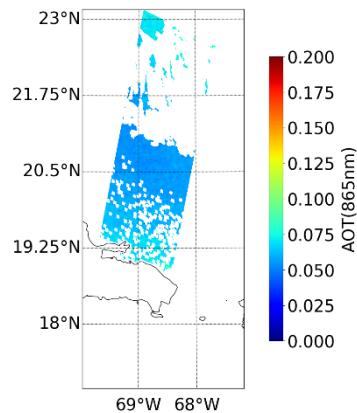
retrieved AOT 670 nm



true AOT 865 nm

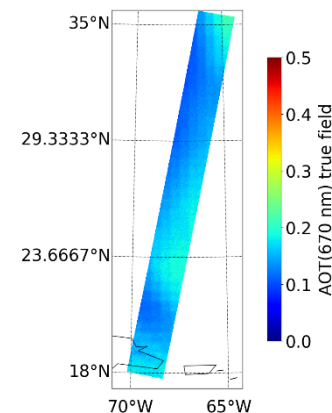


retrieved AOT 865 nm

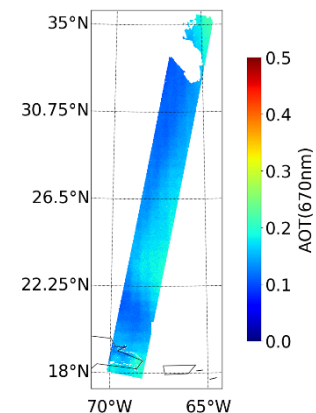


Halifax Aerosol MSI_RGR_1C v 20191029

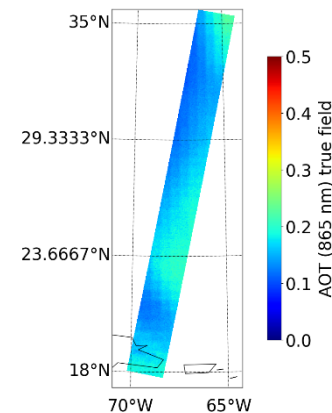
true AOT 670 nm



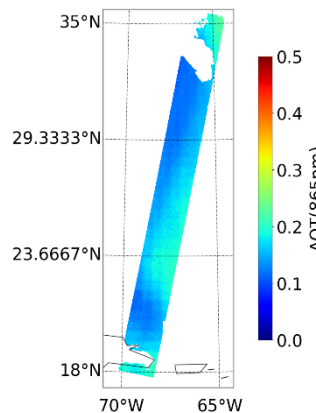
retrieved AOT 670 nm



true AOT 865 nm

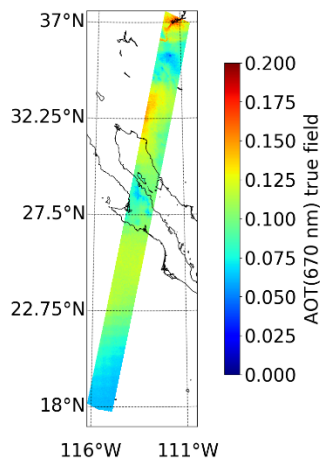


retrieved AOT 865 nm

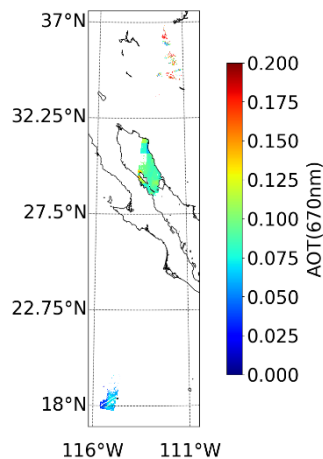


Baja MSI_RGR_1C v 20201125

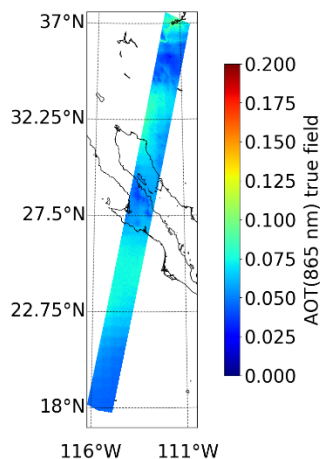
true AOT 670 nm



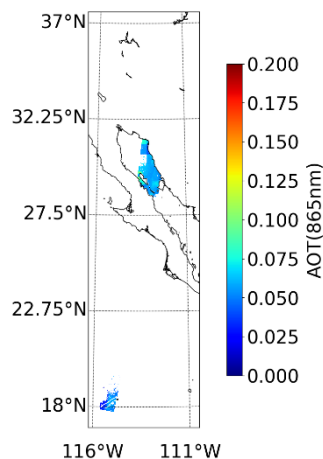
retrieved AOT 670 nm



true AOT 865 nm

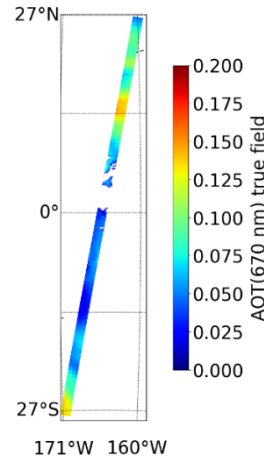


retrieved AOT 865 nm

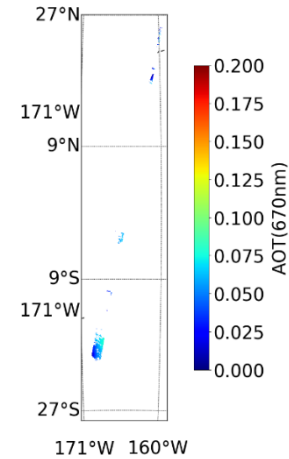


Hawaii MSI_RGR_1C v 20201026

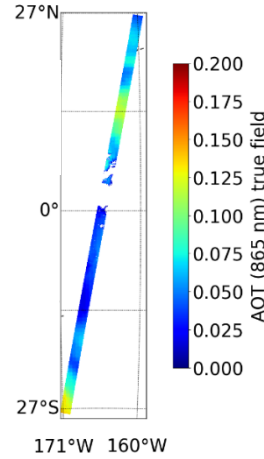
true AOT 670 nm



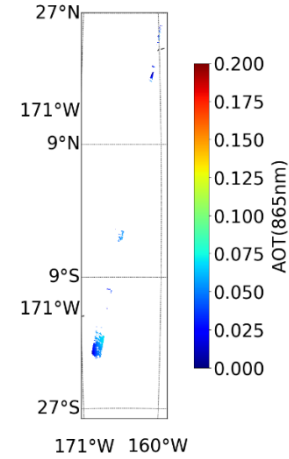
retrieved AOT 670 nm



true AOT 865 nm



retrieved AOT 865 nm



- M-AOT processor creates the M-AOT product
 - aerosol optical thickness retrieval over ocean and, where possible, land that uses multi-spectral imager measurements assuming one central wavelength per VNS band
 - Optimal estimation based approach used
 - Usage of HETEAC based aerosol classification in M-AOT LUTs to ensure consistency between instruments
 - Usage of land surface parameterization that is based on MODIS BRDF / albedo climatology
-
- M-AOT has been tested with ECSIM and MODIS based inputs
 - Verification using true fields of ECSIM simulations and the operational MODIS product and AERONET/MAN AOTs are underway